

Summary for OWB ISC-PRIME modeling, Round 2

"Two-foot-above-roofline analysis"

Test cases were largely modeled upon assumptions used in 2006 NYSDEC modeling

PM_{2.5} modeling performed for 24-hour averaging period only

Predicted modeling impacts were compared to 21 $\mu\text{g}/\text{m}^3$, (the federal standard of 35 $\mu\text{g}/\text{m}^3$ minus the rural background value for Central Maine (14 $\mu\text{g}/\text{m}^3$)

Given the large variation of terrain in Maine, flat terrain was assumed.

Receptor Grid

Polar grid receptor placement every 10 degrees at the following spacing:

10 meter spacing from 0 to 200 meters
50 meter spacing from 200 to 500 meters
100 meter spacing from 500 to 1000 meters

Stack Parameters

Stack Heights: 18 feet, 24 feet, 30 feet
Stack Diameter: 0.66 feet (8 inches, suggested to be the industry standard)
Stack Temp: 294° F (418.71K), acceptable range 300° – 500° F
Stack Velocity: 3.44 feet/sec (1.05 m/s), number more likely to be in the vicinity of 2-4 m/s, but using 1.05 m/s will add conservatism

Building Downwash

OWB modeled as a 4 foot x 6 foot x 6.5 foot structure

3 house configurations:

Ranch (1 story): 40 feet long x 28 feet wide x 16 feet high
Cape (1 ½ stories): 40 feet long x 28 feet wide x 22 feet high
Colonial (2 stories): 40 feet long x 28 feet wide x 28 feet high

OWB Stack was assumed to be located on OWB within 20 feet of buildings

Meteorological Data

5/30/07

5 years of hourly Augusta meteorological data, 1984-1988

Emission Rate

3 different emission rates (g/s):

- 120 grams/hour (0.0333 g/s) – Current reasonable actual “upper limit” OWB emission rate, based upon manufacturers data and recommendations
- 60 grams/hour (0.0167 g/s) – just below Phase I upper limit of 70 grams/hour
- 15 grams/hour (0.0042 g/s) – Phase II limit

Conclusions

Furthest modeled distance (for all H8H modeling runs) to reach $< 21 \mu\text{g}/\text{m}^3$ was 361 feet, based upon the current 120 g/h emission rate and 18' stack (with structure present). Some setback to be required for all 120 g/h cases.

The presence of buildings greatly affects the local dispersion pattern, regardless of stack height. The two-feet-above-roofline assumption doesn't appear to have made any real improvement in final results (compared to previous modeling). The reduction in emission rate is more of the driving factor.

When structures were present, the maximum H8H impact of almost every model runs occurred very close to the stack/boiler, due to low stack velocity/building downwash.

5-30-07

ISC-PRIME OWB MODEL RESULTS, 3 SCENARIOS (120, 60, 15 grams/hour), 3 STACK HEIGHTS (18, 24, 30 feet)

| SCENARIO #1 | | 120 grams/hour | | 60 grams/hour | | 15 grams/hour | |
|---|----------|--------------------------|---|--------------------------|---|---------------------------|---|
| Stack Height (ft) | MET YEAR | 0.0333 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.0167 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.00417 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 |
| 18.00 | 1984 | 49.51 | 98 | 24.83 | 66 | 6.20 | 0 |
| | 1985 | 56.05 | 131 | 28.11 | 66 | 7.02 | 0 |
| Building Type (ft) 28x40x16 Ranch | 1986 | 52.09 | 98 | 26.12 | 66 | 6.52 | 0 |
| | 1987 | 51.20 | 361 | 25.68 | 66 | 6.41 | 0 |
| | 1988 | 49.49 | 98 | 24.82 | 66 | 6.20 | 0 |

| SCENARIO #2 | | 120 grams/hour | | 60 grams/hour | | 15 grams/hour | |
|--|----------|--------------------------|---|--------------------------|---|---------------------------|---|
| Stack Height (ft) | MET YEAR | 0.0333 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.0167 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.00417 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 |
| 24.00 | 1984 | 36.70 | 98 | 18.40 | 0 | 5.46 | 0 |
| | 1985 | 41.21 | 98 | 20.67 | 0 | 6.29 | 0 |
| Building Type (ft) 28x40x22 Cape | 1986 | 39.22 | 98 | 19.67 | 0 | 6.08 | 0 |
| | 1987 | 38.36 | 98 | 19.24 | 0 | 5.62 | 0 |
| | 1988 | 36.87 | 98 | 18.49 | 0 | 5.60 | 0 |

| SCENARIO #3 | | 120 grams/hour | | 60 grams/hour | | 15 grams/hour | |
|--|----------|--------------------------|---|--------------------------|---|---------------------------|---|
| Stack Height (ft) | MET YEAR | 0.0333 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.0167 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 | 0.00417 g/s Max Impact | Downwind Distance (ft) < 21 ug/m3 |
| 30.00 | 1984 | 27.19 | 98 | 13.64 | 0 | 3.41 | 0 |
| | 1985 | 29.61 | 98 | 14.85 | 0 | 3.71 | 0 |
| Building Type (ft) 28x40x28 Colonial | 1986 | 27.82 | 66 | 13.95 | 0 | 3.48 | 0 |
| | 1987 | 28.61 | 66 | 14.35 | 0 | 3.58 | 0 |
| | 1988 | 26.45 | 66 | 13.26 | 0 | 3.31 | 0 |

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DRAFT SETBACK PROPOSAL

| Emission Limit | Installation Date | Setback | Nearest residence | Stack Height |
|---|---|--------------------------------|--------------------------|--|
| greater than 0.60 MMBTU/hr input | up to April 2008 (except for sell through) | 200 feet nearest property line | greater than 500 feet | 10 feet above ground |
| | | | 200-500 feet | 2 feet higher than peak of structure being served |
| 0.60 to 0.32 pound per MMBTU per hour input | up to April 2010 | 100 feet nearest property line | greater than 300 feet | 10 feet above ground |
| | | | 100-300 feet | 2 feet higher than peak of structure being served |
| less than or equal to 0.32 pound per MMBTU per hour output | anytime | 50 feet nearest property line | greater than 300 feet | 10 feet above ground |
| | | | 50-300 feet | 2 feet higher than peak of structure being served |

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